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Use of Zernike Polynomials and SPGD Algorithm for Measuring the Reflected Wavefronts from the Lens Surfaces

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ABSTRACT— Recently, we have demonstrated a new and efficient method to simultaneously reconstruct two unknown interfering wavefronts. A three-dimensional interference pattern was analyzed and then Zernike polynomials and the stochastic parallel gradient descent algorithm were used to expand and calculate wavefronts. In this paper, as one of the applications of this method, the reflected wavefronts from two surfaces of a spherical lens are experimentally reconstructed.

KEYWORDS: Interference pattern, Lens parameters; SPGD algorithm, Wavefront reconstruction.

I. INTRODUCTION

Various noninterferometric and interferometric methods have already been proposed for wavefront reconstruction because of its importance in a number of fields such as adaptive optics [1], optical testing [2], and microscopy [3]. The most commonly used noninterferometric techniques are based on the transport of intensity equation [4,5], moiré deflectometry [6,7], Shack–Hartmann wavefront sensor [8], pyramid wavefront sensor [9], and Gerchberg–Saxton algorithm [10]. A large variety of interferometric techniques is known, in which the wavefront is reconstructed by processing the interference

patterns, such as shearing interferometry [11], phase conjugating method [12], and interfering with a known reference wavefront [2].

Reconstructing two unknown interfering wavefronts, without the reference wavefront, has already received much attention [13]–[18]. Two reconstructed interfering wavefronts can be applied to simultaneously test two surfaces of an optical element from which the interfering wavefronts are reflected or transmitted, and to find the parameters of an optical element such as the lens [13]. The measurements of lens parameters, such as focal length, radius of curvature, thickness, and refractive index of the lens material as well as the shape of the wavefront produced by a lens, are important for their proper selection in various applications.

Recently, we introduced and implemented a fast and accurate method for reconstructing two unknown interfering wavefronts based on Zernike polynomials and analyzing the interference patterns [17]. Here, we present another experimental verification of the proposed method, as one of its applications. In this application, the reflected wavefronts from two surfaces of a spherical lens are experimentally reconstructed. These reconstructed wavefronts can provide useful

information to find the lens parameters or to test its surface's quality. In the following sections, we briefly describe the proposed method, and then report the experimental results.

II. THEORY

To reconstruct φ_1 and φ_2 , the unknown phase distributions of two interfering waves in the paraxial approximation, we do the following steps:

1- Interference patterns at two parallel planes are recorded. These planes are perpendicular to the average propagation direction of these waves (z-axis) and located at z_1 and z_2 .

2- Analyzing the recorded fringe patterns with a proper method, such as phase shifting and Fourier transform (FT) [2,19], the phase difference distributions (PDDs), $\Delta\varphi_{1\text{exp}} = \varphi_{2z_1} - \varphi_{1z_1}$ and $\Delta\varphi_{2\text{exp}} = \varphi_{2z_2} - \varphi_{1z_2}$ are derived at these two planes. φ_{iz_j} denotes the phase distribution of the i th wave at plane $z = z_j$.

3- φ_{1z_1} is expanded in terms of N Zernike polynomials [20]:

$$\varphi_{1z_1}(r, \theta) = \sum_{i=1}^N a_i Z_i(r, \theta), \quad (1)$$

where a_i is the coefficient of Zernike polynomial $Z_i(r, \theta)$. To start, guess the expansion coefficients, say $a_i = 0$. Therefore, φ_{1z_1} is determined from Eq. (1) and then φ_{2z_1} is obtained by

$$\varphi_{2z_1} = \varphi_{1z_1} + \Delta\varphi_{1\text{exp}}. \quad (2)$$

4- Propagating two obtained wavefronts to the second observation plane at $z = z_2$, φ_{1z_2} and φ_{2z_2} can be reconstructed. Then, the PDD at the second plane is calculated by

$$\Delta\varphi_{2\text{cal}} = \varphi_{2z_2} - \varphi_{1z_2}. \quad (3)$$

5- Cost function C based on the difference between the measured and calculated PDDs ($E = \Delta\varphi_{2\text{exp}} - \Delta\varphi_{2\text{cal}}$) is defined, such that if $E = 0$, then C is minimized. Cost function can be defined as

$$C = \bar{E} = \frac{\sum_{i=1}^K \sum_{j=1}^L E_{ij}}{KL}, \quad (4)$$

or

$$C = \sqrt{\bar{M}} \quad , \quad M = (E - \bar{E})^2, \quad (5)$$

where K and L are the number of pixels along the x and y directions at the observation planes, respectively.

6- The stochastic parallel gradient descent (SPGD) algorithm [21,22] is used to find the optimum Zernike coefficients of φ_{1z_1} in order to minimize the cost function.

III. EXPERIMENTS

A. Experimental details and results

We experimentally reconstructed two interfering wavefronts which were reflected from two surfaces of a spherical lens. A schematic of our experimental setup is shown in Fig. 1. The collimated laser beam with wavelength of 638nm (light source: RO-638-PLR-30, Ondax, USA) was focused by the lens L_1 , and then was reflected from the test lens L_2 (Thorlabs, N-BK7 Plano-Convex Lens, focal length=60mm and diameter=25.4mm). Superimposing two spherical wavefronts, reflected from the surfaces of test lens, produced the required interference field. A camera (lw115, Lumenera Imaging Corp., Canada) was used to record the interference pattern. The camera plane, considered as the x-y plane, was perpendicular to the average propagation direction of wavefronts (z-axis). We displaced the camera

along the z -axis with the precision of 0.01mm and recorded another interference pattern after an arbitrary displacement of $\Delta z = z_2 - z_1 = 3mm$. Finally, we selected a grid with 830×830 pixels from every recorded pattern for analyzing. The selected pattern at the first plane located at $z = z_1$ is shown in Fig. 2. The radial profile of interference intensity was obtained by averaging along every fringe (Fig. 3). The FT method [19] was used to calculate the PDDs at both observation planes. Figures 4 and 5 show the measured PDDs along the radius of fringe patterns at observations planes, and the quadratic curves fitting on them.

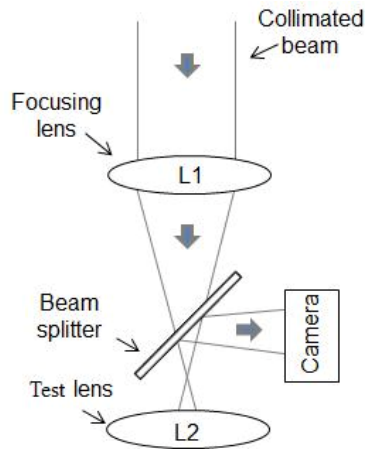


Fig. 1 Schematic diagram of the experimental setup.

In using the FT method to derive the PDD, if the fringe pattern includes low and different spatial frequencies, then its first harmonics in the Fourier space overlap the bias. So, separating the harmonics and consequently reconstructing the PDD are not accurate. To obtain a good result with FT method, a fringe pattern with a high carrier spatial frequency is a good option. Due to the finite aperture of camera and setup situation, if we selected a symmetric interference pattern around the central fringe, we missed the high spatial frequency fringes which were located far from center. This selection could reduce the accuracy of results. This limitation does not exist in the phase shifting method, which works with any fringe pattern. However, we

did not have the required components to implement phase shifting, like a tunable light source.

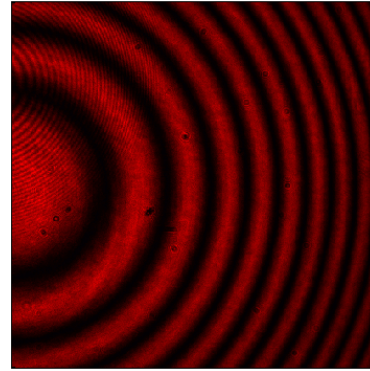


Fig. 2 Interference pattern at the first observation plane.

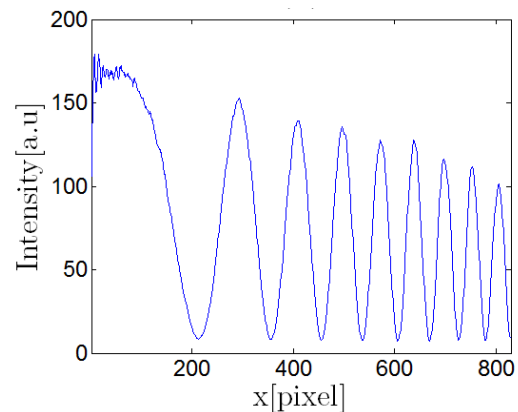


Fig. 3 Radial profile of intensity at the first observation plane.

According to the described technique in Section II, the interfering wavefronts were reconstructed from the PDDs which were multiplied by a circle function with diameter of 830 pixels. To start, a plane wavefront was selected as the initial guess for one of the wavefronts. The coefficients of the first 5 Zernike polynomials and Eq. (5) were considered as the unknown variables and the cost function in the SPGD algorithm, respectively. The ray-tracing method was used for wavefront propagation [23,24]. Figure 6 shows the cost function during the reconstruction process with the solid line. As expected, the cost function decreases with higher iteration number of the algorithm. The

difference between the measured and reconstructed PDDs in the second plane decreases simultaneously. After 350 iterations, the peak to valley (PV) of this difference is 0.37rad which results in a relative error of 0.8% compared to the experimental PDD in the second plane with PV=46.64rad.

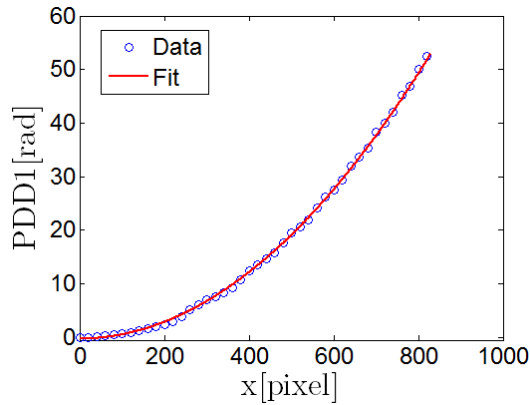


Fig. 4 Measured PDD (circles) and the fitted quadratic curve (solid line) along the radius of fringe pattern at the first observation plane.

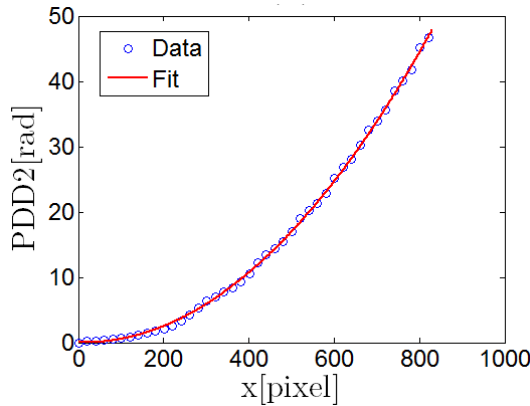


Fig. 5 Measured PDD (circles) and the fitted quadratic curve (solid line) along the radius of fringe pattern at the second observation plane.

The reconstructed phase distributions of interfering wavefronts in the first plane after 350 iterations are shown in Figs. 7 and 8. These results show two spherical wavefronts with different curvatures, which agree well with our predictions and so validate the proposed method.

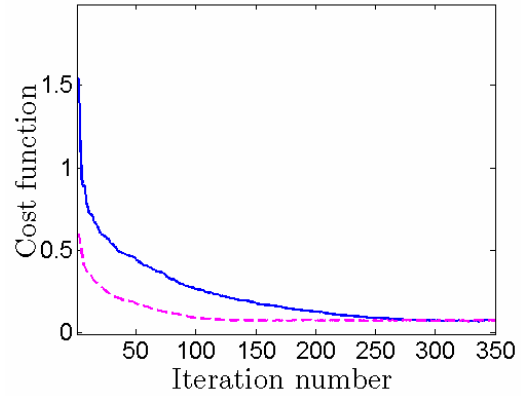


Fig. 6 Cost function during the reconstruction process, when the initial guess for one of the wavefronts is a plane wavefront (solid line) and a spherical wavefront with an arbitrary value of tilt (dashed line).

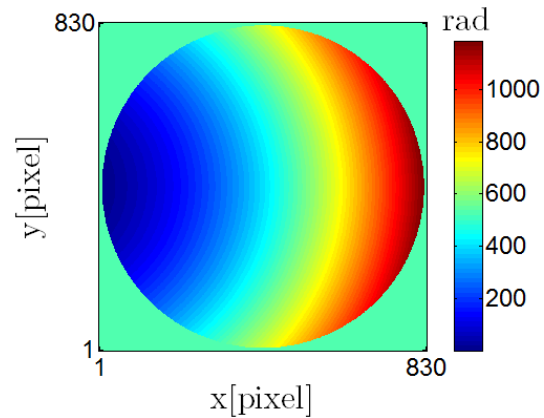


Fig. 7 Reconstructed phase distribution of the first wavefront.

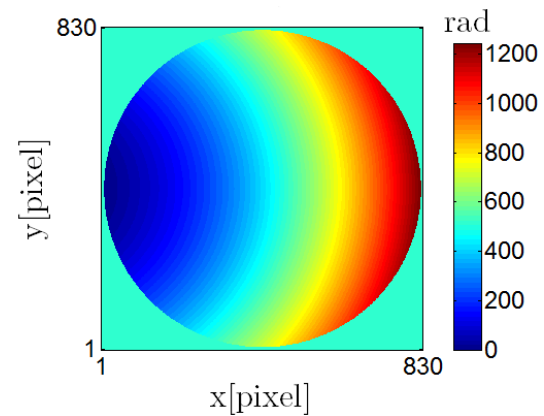


Fig. 8 Reconstructed phase distribution of the second wavefront.

B. Convergence speed of algorithm

In the obtained results, we considered a plane wavefront as the initial guess for one of the wavefronts in the beginning of algorithm. As this guess is close to the real wavefront, the convergence speed of algorithm is much faster. So, in the next step, we selected a spherical wavefront with an arbitrary value of tilt as the initial guess, and repeated the reconstruction process. The decreasing cost function in this case is shown with the dashed line in Fig. 6. Comparing the curves shown in Fig. 6, it is seen that after about 160 iterations, we can get the same results which were obtained after 350 iterations in the first experiment. This result verifies that the convergence speed of algorithm and consequently the reconstruction time are strongly dependent on the initial guess for one of the interfering wavefronts.

IV. CONCLUSION

In this paper, we have simultaneously reconstructed two interfering wavefronts reflected from two surfaces of a lens. These wavefronts can provide the useful information to find the lens parameters, and test the quality of lens surfaces without a reference wavefront. In fact, the deviations in every reconstructed wavefront compared to an ideal spherical wavefront show the aberrations of surface from which the wavefront is reflected. In our results these aberrations disappear because we used the fitted quadratic curves on the PDDs obtained from the FT method. In addition phase shifting with a tunable light source would permit calculation of the surface aberrations.

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